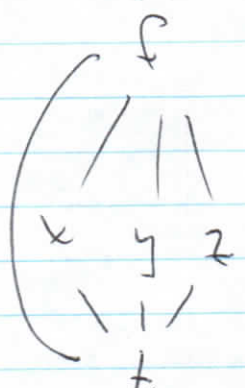


Substantial Derivative

(-2)

Consider the function $f(x, y, z, t)$ where $x(t)$ $y(t)$ $z(t)$

$$\begin{aligned}\frac{df}{dt} &= \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} + \frac{\partial f}{\partial t} \\ &= \underline{v} \cdot \nabla f + \frac{\partial f}{\partial t}\end{aligned}$$


so if $f = \rho \eta$

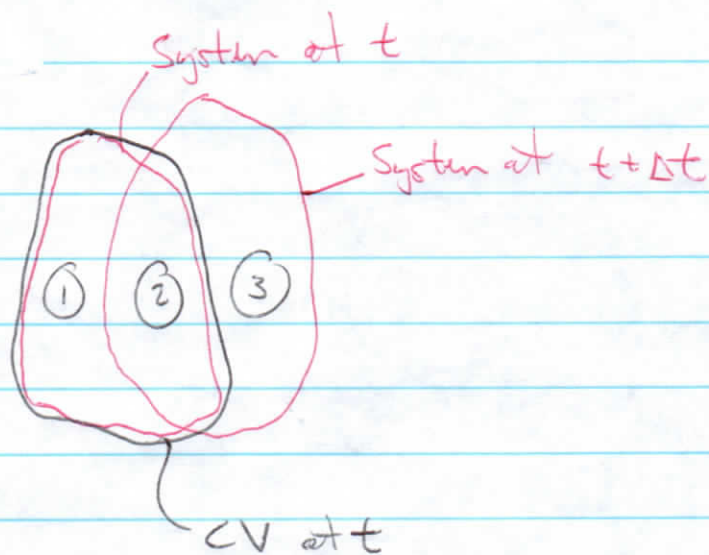
$\rho \sim \text{mass density} \quad \text{m/vol}$
 $\eta \sim \text{stuff/mass}$
 $f \sim \text{stuff/vol}$

$$\frac{d}{dt}(\rho \eta) = \underline{v} \cdot \nabla(\rho \eta) + \frac{\partial}{\partial t}(\rho \eta)$$



Reynolds Transport Thm

3



Look at $\frac{DN_{sys}}{Dt} = \lim_{\Delta t \rightarrow 0} \frac{N_{sys}(t + \Delta t) - N_{sys}(t)}{\Delta t}$

$$= \lim_{\Delta t} \frac{[N_3(t + \Delta t) + N_2(t + \Delta t)] - [N_2(t) + N_1(t)]}{\Delta t}$$

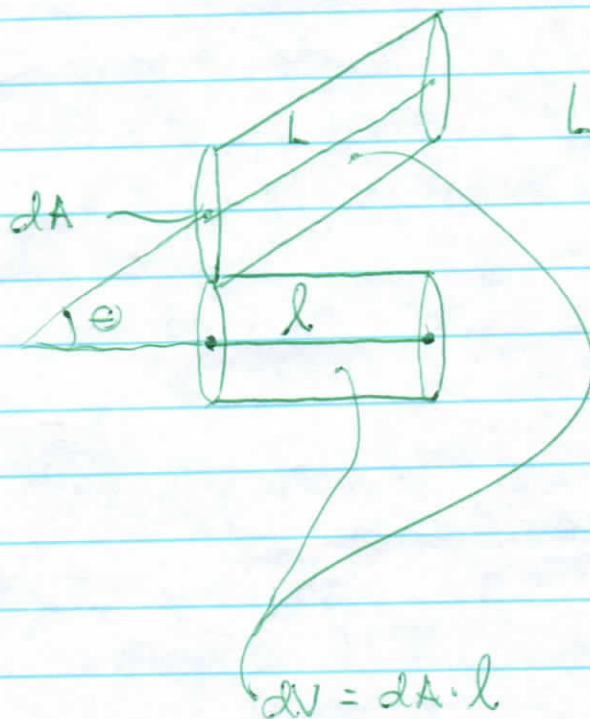
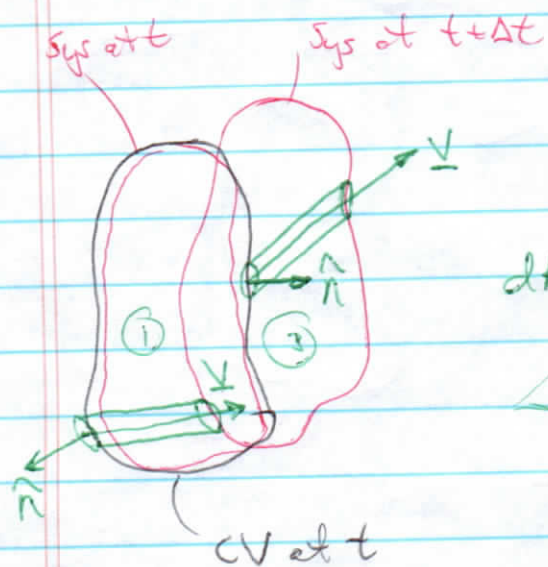
$$= \lim_{\Delta t} \frac{[N_2(t + \Delta t) + \overset{\circledast}{N_1(t + \Delta t)}] - [N_2(t) + N_1(t)] + N_3(t + \Delta t) - \overset{\circledast}{N_1(t + \Delta t)}}{\Delta t}$$

$$= \lim_{\Delta t \rightarrow 0} \frac{N_{cv}(t + \Delta t) - N_{cv}(t)}{\Delta t} + \lim_{\Delta t \rightarrow 0} \frac{N_3(t + \Delta t) - N_1(t + \Delta t)}{\Delta t}$$

$$= \frac{d}{dt} \iiint_{CV} \rho \eta dV + \lim_{\Delta t \rightarrow 0} \frac{N_3(t + \Delta t) - N_1(t + \Delta t)}{\Delta t}$$

lets look at this

(4)



$$L = |\underline{V}| \Delta t$$

$$\begin{aligned} dV &= dA \cdot l \\ &= dA \cdot L \cos \theta \\ &= dA |\underline{V}| \Delta t \cos \theta \\ &= dA \underline{V} \cdot \hat{n} \Delta t \end{aligned}$$

$$\text{So } \frac{N_2(t + \Delta t) - N_1(t + \Delta t)}{\Delta t} = \frac{\iint_{\text{CS}} \rho \underline{V} \cdot \hat{n} dA \Delta t}{\Delta t}$$

$$\therefore \lim_{\Delta t \rightarrow 0} \frac{N_2(t + \Delta t) - N_1(t + \Delta t)}{\Delta t} = \iint_{\text{C.S.}} \rho \underline{V} \cdot \hat{n} dA$$

$\underline{V}$ _{stuff/boundary}

(5)

We are finally left with

$$\frac{D N_{sys}}{Dt} = \frac{d}{dt} \iiint_{CV} \rho \eta dV + \iint_{C.S.} \rho \eta \frac{V_o \hat{n}}{s/b} dA \quad \text{Version 1} \quad (1)$$

Reynolds Transport Thm,

$\underline{V}$ = velocity of stuff
relative to
the boundary
 $= \frac{V}{s/b}$

Can also write this as (using Leibnitz Thm)

$$\frac{d}{dt} \iiint_{CV} \rho \eta dV = \iiint_{CV} \frac{\partial}{\partial t} (\rho \eta) dV + \iint_{C.S.} \rho \eta V_o \hat{n} dA$$

in which case RTT becomes

$$\frac{D}{Dt} N_{sys} = \iiint_{CV} \frac{\partial}{\partial t} (\rho \eta) dV + \iint_{C.S.} \rho \eta (\underline{V}_{s/b} + \underline{V}_{b/o}) \cdot \hat{n} dA \quad \text{Version 2} \quad (2)$$

G.D.T.

$$\iint \underline{F} \cdot \hat{n} d\sigma = \iiint \nabla \cdot \underline{F} dV$$

$$\frac{\partial}{\partial t} \iiint_R \underline{s} dV + \iint_S \underline{s} \cdot \underline{v} \cdot \hat{n} d\sigma = \iiint_R \nabla \cdot (\underline{s} \underline{v}) dV$$

$$\text{let } \underline{F} = \underline{s} \underline{v}$$

Vect. Identity

$$\nabla \cdot (\underline{s} \underline{v}) =$$

$$\underline{s} \nabla \cdot \underline{v} + \nabla \underline{s} \cdot \underline{v}$$

TO Differential Forms

(2)

Conservation of mass.

$$\frac{DM_{\text{mass}}}{Dt} = 0 = \iiint \frac{\partial s}{\partial t} dt + \iint s \frac{\underline{V} \cdot \hat{n}}{s_0} d\sigma$$

G. Div. Thm. $\iint \underline{F} \cdot \hat{n} d\sigma = \iiint \nabla \cdot \underline{F} dt$

$$\iiint \nabla \cdot (s \underline{V}) dt$$

$$0 = \iiint_{CV} \left[\frac{\partial s}{\partial t} + \nabla \cdot (s \underline{V}) \right] dt$$

but the CV was arbitrary so the integrand must be 0 any/every where

$$\therefore \boxed{\frac{\partial s}{\partial t} + \nabla \cdot (s \underline{V}) = 0} \quad \text{Cons. of mass}$$

$$\downarrow$$
$$= \nabla s \cdot \underline{V} + s \nabla \cdot \underline{V}$$

$$\frac{\partial s}{\partial t} + \nabla s \cdot \underline{V} + s \nabla \cdot \underline{V} = 0$$

$$\boxed{\frac{Ds}{Dt} + s \nabla \cdot \underline{V} = 0}$$

CONS. OF MASS

For solids + fluids $s \approx \rho$

reduces to $\nabla \cdot \underline{V} = 0$

To look at (mom) + (E) + (S) first later
rewrite RTT's ~~left hand side~~ RHS

$$\frac{DN_{sys}}{Dt} = \iiint_{CV} \frac{\partial s\eta}{\partial t} dV + \iiint_{CS} s\eta \underline{V} \cdot \underline{\hat{n}} d\sigma$$

G.D.Th.

$$= \iiint_{CV} \left[\frac{\partial s\eta}{\partial t} + \nabla \cdot (s\eta \underline{V}) \right] dV$$

$$= \iiint_{CV} \left[\frac{\partial s\eta}{\partial t} + s\eta \nabla \cdot \underline{V} + (\nabla s\eta) \cdot \underline{V} \right] dV$$

$$= \iiint_{CV} \left[\frac{Ds\eta}{Dt} + s\eta \nabla \cdot \underline{V} \right] dV$$

$$= \iiint_{CV} \left[s \frac{D\eta}{Dt} + \frac{Ds}{Dt} \eta + s\eta \nabla \cdot \underline{V} \right] dV$$

$$= \iiint_{CV} \left[s \frac{D\eta}{Dt} + \eta \left(\frac{Ds}{Dt} + s \nabla \cdot \underline{V} \right) \right] dV$$

= 0 by (m)

$$\boxed{\frac{DN_{sys}}{Dt} = \iiint_{CV} s \frac{D\eta}{Dt} dV}$$

We will use this for
the rest of this on
the RHS of (x-mom) (E)

(E)

4

$$\frac{D\bar{E}_{\text{sys}}}{Dt} = \underbrace{\iiint \frac{\partial \bar{e}}{\partial t} d\tau}_{\downarrow} + \underbrace{\iint_{CS} \bar{e} \underline{V} \cdot \hat{n} d\sigma}_{\rightarrow}$$

$$-\iint_{CS} \bar{g} \cdot \hat{n} d\sigma - \iint_{CS} p \underline{V} \cdot \hat{n} d\sigma + \iint_{CV} U'' d\tau = \iiint_{CV} \bar{e} \frac{D\bar{e}}{Dt} d\tau$$

Turn surface integrals into volume integrals

$$-\iiint \nabla \cdot \bar{g} d\tau - \iiint \nabla \cdot (p \underline{V}) d\tau + \iiint U'' d\tau = \iiint \bar{e} \frac{D\bar{e}}{Dt} d\tau$$

$$\text{or } \iiint [] d\tau = 0 \Rightarrow [] = 0$$

so

$$\bar{e} \frac{D\bar{e}}{Dt} + \nabla \cdot (\bar{g} + p \underline{V}) = U''$$

But $\bar{e} = U + \frac{V^2}{2} + gz$ so we are going to break this up into mech energy + thermal energy...

$$\bar{e} \frac{D\bar{e}}{Dt} + \underbrace{\nabla \cdot \left(\frac{V^2}{2} + gz \right)}_{\text{mech}} + \underbrace{\nabla \cdot \bar{g} + \nabla \cdot (p \underline{V})}_{\text{mech}} = U''$$

so

$$\boxed{\bar{E}_{\text{thermal}} \left[\bar{e} \frac{D\bar{e}}{Dt} + \nabla \cdot \bar{g} = U'' \right]}$$

and the rest of it is actually Bernoulli's eqn!

Finally we use $du = C_v dT$ heat cap. def.

$$\underline{\bar{g}} = -k \nabla T \quad \text{Fourier's Law}$$

5

$$\rho \frac{Dc_p T}{Dt} = \nabla \cdot (k \nabla T) + \dot{q}'''$$

If $c_p = \text{const}$ and $k = \text{const}$ ($c_p \approx c_p = c$ for solids & liquids)

$$\rho c \frac{DT}{Dt} = k \nabla^2 T + \dot{q}'''$$

Classic heat
cond. eqn for (E)

$$\rho c \left(\frac{\partial T}{\partial t} + \mathbf{V}_0 \cdot \nabla T \right) = k \nabla^2 T + \dot{q}'''$$